

Electrical Machines

Answer Keys and Explanations

- [Ans. B]**
(Transformer B has more weight than A)
Since, both are connected to the same bus bar so both will have same voltage, 'V' applied
 $V \propto \phi$, so flux is also constant in both transformers
Now, $\phi = B.A$, B → flux density
A → Area of core
 $B \propto \frac{1}{A} \therefore \phi = \text{Constant}$
 \therefore Area of transformer A core is less than that of B. So weight of transformer B is more than A.
- [Ans. C]**
- [Ans. *] Range: 0.955 to 0.965**
Number of slots per pole per phase = $g' = 3$.
With 3 phase, number of slots per pole = $g \times 3 = 9$. Slot pitch $\Psi = \frac{180^\circ}{9} = 20^\circ$ elec
For 60° phase spread double layer winding, distribution factor is given by
 $k_d = \frac{\sin g' \frac{\Psi}{2}}{g' \sin \frac{\Psi}{2}} = \frac{\sin \frac{3 \times 20^\circ}{2}}{3 \sin \frac{20^\circ}{2}} = \frac{\sin 30^\circ}{3 \sin 10^\circ} = 0.96$
- [Ans. *] Range 600 to 600**
For convenience let the slope of the linear portion of OCC = m .
 m is directly proportional to the speed of the rotor. Operating as a shunt generator, m must be greater than or equal to the field circuit resistance for buildup, the quality giving the critical speed at 1500 RPM, $m = 250$ (given)
For $m = 100$, Speed = $\frac{100}{250} \times 1500 = 600$ RPM
- [Ans. D]**
Method 1:
Supply voltage $V_1 = 800V$
Primary turns $N_1 = 1250$
Secondary turns $N_2 = 800$
Secondary voltage $V_2 = V_1 \times \frac{N_2}{N_1} = 250 \times \frac{800}{1250} = 160V$
Method 2:
EMF per turn = $\frac{V_1}{N_1} = \frac{250}{1250} = 0.2V$
And secondary voltage $V_2 = \text{EMF per turn} \times \text{secondary turns} = 0.2 \times 800 = 160V$

6. [Ans. *] Range 210 to 212

Main winding impedance, $Z_m = (4.5 + j3.7)\Omega$ or $5.826\angle 39.43^\circ\Omega$

Main winding current, I_m lags behind the applied V by 39.43°

Auxiliary winding impedance, $Z_a = (9.5 + j3.5)\Omega$

Since, time phase angle between auxiliary winding current I_a is 90° , so auxiliary winding current I_a must lead the applied voltage by $(90^\circ - 39.43^\circ)$ or 50.57° .

If X_c is the capacitive reactance of the capacitor connected in series with the auxiliary winding, then impedance of the auxiliary winding will be given as

$Z_a = (9.5 + j3.5 - jX_c)$ or $[9.5 + j(3.5 - X_c)]\text{ohm}$

For auxiliary winding,

$$\tan \phi_m = \frac{3.5 - X_c}{9.5}$$

$$\Rightarrow X_c = 3.5 - 9.5 \tan \phi_a = 3.5 - 9.5 \tan(-50.57)^\circ$$

$$= 3.5 + 11.553 = 15.053\Omega$$

$$\text{Capaitance, } C = \frac{1}{2\pi f X_c} = \frac{1}{2\pi \times 50 \times 15.053} = 211.5\mu\text{F}$$

7. [Ans. D]

$$T_s = 1.5T_f$$

$$T_{\max} = 2T_f$$

For maximum torque, $s_{mT} = \frac{r_2}{X_2}$

$$\frac{T_s}{T_{\max}} = \frac{1.5T_f}{2T_f} = \frac{2s_{mT}}{1 + s_{mT}^2}$$

$$\text{i. e., } 1.5 s_{mT}^2 4s_{mT} + 1.5 = 0$$

$$\therefore s_{mT} = 0.45$$

$$\text{also, } \frac{T_f}{T_{\max}} = \frac{T_f}{2T_f} = \frac{2s_{mT}}{s_{mT}^2 + s^2}$$

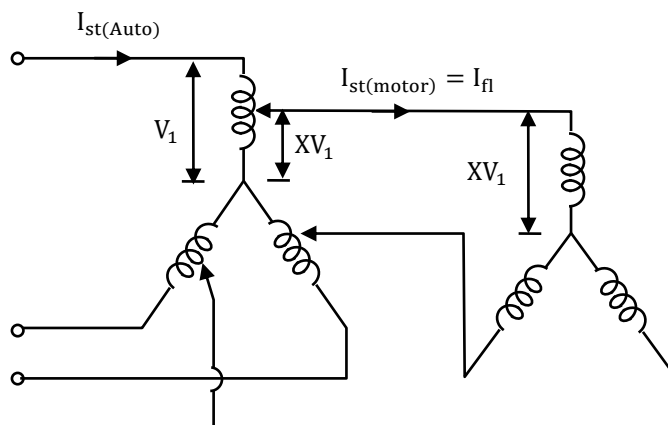
at $s_{mT} = 0.45$,

$$s^2 - 4s_{mT}s + s_{mT}^2 = 0$$

$$\Rightarrow s^2 - 4(0.45)s + (0.45)^2 = 0$$

$$s = 0.12$$

8. [Ans. *] Range 141 to 143



$$x = 60\% = 0.6$$

$$I_{fl(\text{motor})} = \frac{50 \times 10^3}{\sqrt{3} \times 440} = 65.61 \text{ a}$$

$$I_{st(\text{motor})} = 6I_{fl} = 6 \times 65.61 \text{ A} = 393.65 \text{ a}$$

$$\begin{aligned} I_{st(\text{Auto})} &= x^2 I_{st(\text{motor})} \\ &= (0.6)^2 \times 393.65 \text{ a} \\ &= 141.71 \text{ A} \end{aligned}$$

9. **[Ans. *] Range 15 to 16**

$$N_s = \frac{120f_1}{P} = \frac{120 \times 50}{6} = 1000 \text{ rpm}$$

$$s = \frac{f_2}{f_1} = \frac{1.5}{50} = 0.03 \text{ or } 3\%$$

$$N_r = (1 - s)N_s = (1 - 0.03) \times 1000 = 970 \text{ rpm}$$

$$\omega_r = 2\pi N_r = \frac{2\pi \times 970}{60} = 101.58 \text{ rad/s}$$

$$\begin{aligned} \text{Shaft power output } P &= T\omega_r \\ &= 150 \times 101.58 = 15236 \text{ W} = 15.236 \text{ kW} \end{aligned}$$

10. **[Ans. A]**

$$f_1 = \frac{PN_s}{120}$$

$$50 = \frac{6 \times N_s}{120}, N_s = \frac{120 \times 50}{6} = 1000 \text{ rpm}$$

$$s = \frac{N_s - N_r}{N_s} = \frac{1000 - 960}{1000} = 0.04 \text{ p. u.}$$

$$\text{Rotor copper loss} = \frac{s}{1 - s} \times \text{Mechanical power developed}$$

$$3I_2^2 R_2 + 250 = \frac{0.04}{1 - 0.04} (25 \times 746 + 1000)$$

$$3 \times 35^2 R_2 = 818.75 - 250$$

$$R_2 = \frac{568.75}{3 \times 35^2} = 0.154 \Omega$$